

## Cylindrical waveguides, plane waves

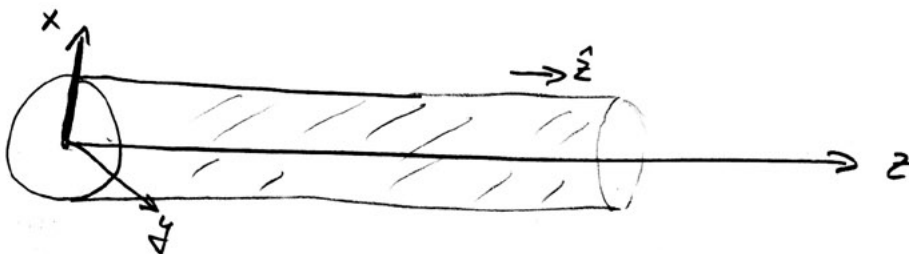
Again Maxwell equations:

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} = i\omega \vec{B}$$

$$\nabla \times \vec{B} = \frac{1}{v^2} \frac{\partial \vec{E}}{\partial t} = -i\epsilon\mu\omega \vec{E}$$

$$\nabla \cdot \vec{E} = 0, \quad \nabla \cdot \vec{B} = 0$$

↳ wave equation:  $[\Delta + \mu\epsilon\omega^2](\vec{E}, \vec{B}) = 0$



for wave traveling in z-directions:  $\vec{E} = \vec{E}(x,y) e^{i(kz - \omega t)}$

↳ 
$$\left[ \underbrace{\left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right)}_{\Delta_{xy}} + (\mu\epsilon\omega^2 - k^2) \right] \begin{pmatrix} E \\ B \end{pmatrix} = 0 \quad \left| \begin{array}{l} \text{two-dimensional} \\ \text{DE} \end{array} \right.$$

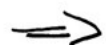
Next: split  $\vec{B}, \vec{E}$ -field components in  $\parallel$  and transverse components

$$\vec{E} = \vec{E}_z + \vec{E}_t = E_z \hat{z} + (\hat{z} \times \vec{E}) \times \hat{z}$$

$$\vec{B} = \vec{B}_z + \vec{B}_t = B_z \hat{z} + (\hat{z} \times \vec{B}) \times \hat{z}$$

↳ Maxwell equ.:  $\frac{\partial E_t}{\partial z} + i\omega \hat{z} \times \vec{B}_t = \nabla_t E_z; \quad \nabla_t = \left( \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, 0 \right)$

$$\frac{\partial B_t}{\partial z} - i\mu\epsilon\omega \hat{z} \times \vec{E}_t = \nabla_t B_z$$



$$\hat{z} \cdot (\nabla_t \times \vec{E}_t) = i\omega B_z, \quad \hat{z} \cdot (\nabla_t \times \vec{B}_t) = -i\mu\epsilon\omega E_z$$

$$\nabla_t \cdot \vec{E}_t = -\frac{\partial E_z}{\partial z}, \quad \nabla_t \cdot \vec{B}_t = -\frac{\partial B_z}{\partial z}$$

↳ Solutions: 
$$E_t = \frac{i}{\mu\epsilon\omega^2 - k^2} [k \cdot \nabla_t E_z - \omega \hat{z} \times \nabla_t B_z]$$

$$B_t = \frac{i}{\mu\epsilon\omega^2 - k^2} [k \cdot \nabla_t B_z + \mu\epsilon\omega \hat{z} \times \nabla_t E_z]$$

Transverse electromagnetic wave (TEM-wave):

\* only field-components transverse to propagation direction

$$E_z = 0, \quad B_z = 0 \quad \leadsto \quad \boxed{E_t = E_{TEM}}$$

with  $\boxed{\nabla_t \times E_{TEM} = 0}$  and  $\boxed{\nabla_t \cdot E_{TEM} = 0}$

↳ TEM is solution of electrostatic problem in 2-dim (x-y-plane).

wave vector  $k = k_0 = \frac{\omega}{v_{TEM}}$

$$B_{TEM} = \sqrt{\mu\epsilon} \hat{z} \times \vec{E}_{TEM}$$

TM-wave: transverse electromagnetic wave

additional boundary value:  $E_z|_{\text{surface}} = 0 \quad (B_z \neq 0)$

while for TE wave:  $\frac{\partial B_z}{\partial n}|_{\text{surface}} = 0, \quad (E_z \neq 0)$

⇒

Wave Impedance  $Z$ :

found via  $H_t = \frac{1}{Z} \hat{z} \times \vec{E}_t$

$$\text{with } Z = \begin{cases} k/\epsilon \cdot \omega = k/k_0 \cdot \sqrt{\mu/\epsilon'} & \text{for TM-wave} \\ \frac{\mu \omega}{k} = k_0/k \cdot \sqrt{\mu/\epsilon'} & \text{for TE wave} \end{cases}$$

$(k_0 = \omega \cdot \sqrt{\mu \epsilon'})$

Rewrite solutions  $E_t, B_t$  (page 65) for TE and TM waves

$$E_t = \frac{i}{\underbrace{\mu \epsilon \omega^2 - k^2}_{\gamma^2}} k \cdot \nabla_t E_z = \frac{i k}{\gamma^2} \nabla_t \psi \quad \left| \quad \psi \cdot e^{i k z} = E_z(H_z) \right.$$

$$H_t = \frac{i k}{\gamma^2} \nabla_t \psi$$

with  $\psi$  has to satisfy  $\left[ \underbrace{\left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right)}_{\Delta_t} + \gamma^2 \right] \psi = 0$

with boundary condition  $\psi|_S = 0$  (TM) or  $\frac{\partial \psi}{\partial n}|_S = 0$  (TE)

$\gamma^2$  has to be  $\geq 0$

$\hookrightarrow$  dimension of waveguide generates discrete eigenvalues  $\gamma_\lambda^2$   
corresponding to  $\psi_\lambda$ ,  $\lambda = 1, 2, \dots \Rightarrow$  modes of guide

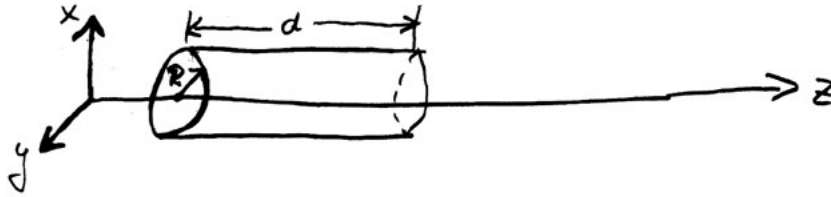
For a given frequ.  $\omega$ :  $k_\lambda^2 = \mu \epsilon \omega^2 - \gamma_\lambda^2$  with cutoff frequ.  $\omega_\lambda = \frac{\gamma_\lambda}{\sqrt{\mu \epsilon'}}$

$\hookrightarrow k_\lambda = \sqrt{\mu \epsilon'} \cdot \sqrt{\omega^2 - \omega_\lambda^2}$ ,  $[\omega > \omega_\lambda: k_\lambda \text{ - real } \leadsto \text{ wave can propagate}]$

phase velocity  $v_p = \frac{\omega}{k_\lambda} = \frac{1}{\sqrt{\mu \epsilon'}} \cdot \frac{1}{\sqrt{1 - (\omega_\lambda/\omega)^2}} > \frac{1}{\sqrt{\mu \epsilon'}}$

## Resonant Cavities

Cylindrical cavity with plane end caps



- walls of cavity has infinite conductivity
- inside cavity is filled with lossless dielectric  $\epsilon, \mu$

↳ Reflection on end surfaces ( $z$ -direction) generates standing waves:

$$A \cdot \sin(k \cdot z) + B \cos(k \cdot z)$$

Boundary condition: 1<sup>st</sup>-cap @  $z=0$ , 2<sup>nd</sup>-cap @  $z=d$

$$\text{↳ } k = p \cdot \frac{\pi}{d} \quad (p = 0, 1, \dots)$$

For TM-field ( $E_z|_{z=0} = 0$  and  $E_z|_{z=d} = 0$ ):

$$E_z = \psi(x, y) \cdot \cos\left(\frac{p \cdot \pi \cdot z}{d}\right) \quad p = 0, 1, 2, \dots$$

Similarly for TE-field ( $H_z|_{z=0} = 0$ ;  $H_z|_{z=d} = 0$ )

$$\text{↳ } H_z = \psi(x, y) \cdot \sin\left(\frac{p \cdot \pi \cdot z}{d}\right) \quad p = 0, 1, 2, \dots$$

The original solution:  $E_t = \frac{i \cdot k}{\gamma^2} \nabla_t \psi \rightarrow E_t = -\frac{p \cdot \pi}{d \cdot \gamma^2} \sin\left(\frac{p \cdot \pi \cdot z}{d}\right) \nabla_t \psi$   
 (TM-field)

$$H_t = \frac{i \epsilon \omega}{\gamma^2} \cos\left(\frac{p \cdot \pi \cdot z}{d}\right) \cdot \hat{z} \times \nabla_t \psi$$

⇒

→ and for TE-fields:

$$E_t = -\frac{i\omega\mu}{\gamma^2} \sin\left(\frac{p\pi}{d} \cdot z\right) \cdot [\hat{z} \times \nabla_t \psi]$$

$$H_t = \frac{p\pi}{d\gamma^2} \cos\left(\frac{p\pi}{d} \cdot z\right) \cdot \nabla_t \psi$$

which satisfy the boundary conditions at the ends of the cavity.

Still to be solved: Eigenvalue problem for  $\psi$ :

$$[\nabla_t^2 + \gamma^2] \psi = 0$$

with  $\gamma^2$  is now:  $\gamma^2 = \mu\epsilon\omega^2 - \left(\frac{p\pi}{d}\right)^2$  before:  
 $\mu\epsilon\omega^2 - k^2$

For each value of  $p$ ,  $\gamma^2$  determines an eigenfrequ.  $\omega_{zp}$  = Resonance frequencies

$$\text{with } \omega_{zp} = \frac{1}{\sqrt{\mu\epsilon}} \left[ \gamma^2 + \left(\frac{p\pi}{d}\right)^2 \right]$$

and the corresponding fields of that mode.

↳ Resonance frequencies form discrete set:

demanding that  $k = p\pi/d$



Find  $\psi$  for cylinder with radius  $R$  for a TM-mode:

→  $\psi = E_z$  subject to boundary condition  $E_z = 0$  at  $\rho = R$

$$\text{↳ } \psi(\rho, \phi) = E_0 J_m(\gamma_{mn}\rho) e^{\pm im\phi}$$

$$\text{with } \gamma_{mn} = \frac{x_{mn}}{R}$$

⇒

$x_{mn}$  is the  $n$ -th root of  $J_m(x) = 0$ .

$$\begin{bmatrix} m = 0, 1, 2, \dots \\ n = 1, 2, 3, \dots \end{bmatrix}$$

↑ Bessel function (page 114, Jackson)

↳ resonance frequencies  $\omega_{mnp} = \frac{1}{\sqrt{\mu\epsilon}} \cdot \sqrt{\frac{x_{mn}^2}{R^2} + \frac{p^2\pi^2}{d^2}}$

lowest TH-mode:

$$m=0, n=1, p=0 : TH_{010} \quad \omega_{010} = \frac{2.405}{\sqrt{\mu\epsilon} \cdot R}$$

↳ fields  $E_z = E_0 \cdot J_0\left(\frac{2.405}{\sqrt{\mu\epsilon} \cdot R}\right) \cdot e^{-i\omega t}$

$$H_\phi = -i \sqrt{\frac{\epsilon}{\mu}} E_0 J_1\left(\frac{2.405}{\sqrt{\mu\epsilon} \cdot R}\right) e^{-i\omega t}$$

The resonance frequency for this mode is independent of  $d$ .  $\rightarrow$  tuning is not possible!

Solution of  $\psi$  for TE-mode:

$$\psi = H_z \text{ subject to boundary condition on } H_z : \frac{\partial \psi}{\partial \rho} \Big|_R = 0$$

↳ same solution as before

$$\psi(\rho, \phi) = E_0 J_m(\gamma_{mn} \rho) e^{\pm im\phi}$$

$$\gamma = \frac{x'_{mn}}{R}$$

$$x'_{mn} \text{ is } n\text{-th root of } J'_m(x) = 0 \quad \rightarrow$$

Roots of  $J_m'(x) = 0$

$$m=0 \quad \leadsto \quad x'_{0n} = 3.832, 7.016, 10.173$$

... see Jackson p. 370

$\hookrightarrow$  resonance frequencies

$$\omega_{mnp} = \frac{1}{\sqrt{\mu\epsilon}} \left( \frac{x_{mn}^2}{R^2} + \frac{p^2 \pi^2}{d^2} \right)^{1/2} \quad \left| \begin{array}{l} m = 0, 1, 2, \dots \\ n, p = 1, 2, 3, \dots \end{array} \right.$$

lowest TE-mode  $m=n=p=1 \quad \therefore \quad TE_{111}$

$$\leadsto \omega_{111} = \frac{1.841}{\sqrt{\mu\epsilon} \cdot R} \cdot \left( 1 + 2.912 \frac{R^2}{d^2} \right)^{1/2}$$

$\hookrightarrow$  fields:

$$\Psi = H_z = H_0 J_1 \left( \frac{1.841 \cdot R}{R} \right) \cdot \cos \phi \sin \left( \frac{\pi}{d} \cdot z \right) e^{-i\omega t}$$

For  $d$  large enough:  $d > 2.03 R$

$$\omega_{111} < \omega_{010} \text{ (TM-mode)}$$

$\leadsto TE_{111}$  is fundamental oscillation in cavity

Since  $\omega_{mnp|TE}$  depends on ratio  $\frac{d}{R} \leadsto$  tuning is possible!

## Power loss in a Cavity ( $Q$ of cavity)

Waveguides & Resonant Cavity have discrete oscillation frequency defined by geometry of guide.  $\leadsto$  resonance frequencies ( $\omega_j$ )

A wave with frequency  $\omega \neq \omega_j$  will experience power loss by dissipation of energy in cavity wall and/or dielectric.

A measure to  $Q := \omega_0 \cdot \frac{\langle \text{Stored Energy} \rangle_t}{\langle \text{Energy loss per cycle} \rangle_t}$

Power dissipation  $\rightarrow$  in ohmic loss = - time rate of change of stored energy  $U$

$$\hookrightarrow \frac{dU}{dt} = -\frac{\omega_0}{Q} U$$

$$\hookrightarrow U(t) = U_0 e^{-\frac{\omega_0 t}{Q}} \quad \text{which is}$$

the damping of EM-wave

$$E(t) = E_0 e^{-\omega_0 t/Q} \cdot e^{-i(\omega_0 + \Delta\omega)t} \quad (\text{just oscillating part})$$

This damped oscillation is a superposition of frequencies around

$\omega_0 + \Delta\omega$ , which can be written as

$$E(t) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} E(\omega) e^{-i\omega t} d\omega$$

$$\uparrow \quad \quad \quad \uparrow$$

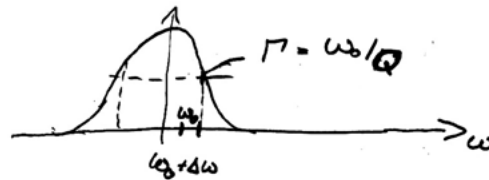
$$L = \frac{1}{\sqrt{2\pi}} \int_0^{\infty} E_0 e^{-\omega_0 t/Q} \cdot e^{i(\omega - \omega_0 - \Delta\omega) \cdot t} dt$$

$\hookrightarrow$  Frequency distribution for the energy in cavity

$$|E(\omega)|^2 \sim \frac{1}{(\omega - \omega_0 - \Delta\omega)^2 + (\omega_0/2Q)^2} \quad \Rightarrow$$



Resonance shape



$\Gamma$ : = full-width at half maximum

$\hookrightarrow Q = \frac{\omega_0}{\Gamma} = \frac{\omega_0}{\delta\omega}$  ← frequency separation

To determine Q :- compute  $\langle \text{energy stored} \rangle_t$   
- determine power loss in the walls.

$\hookrightarrow$  Energy stored:

TH-mode:  $U = \frac{\epsilon}{4} E \left[ 1 + \left( \frac{\rho\pi}{\delta^2\lambda} d \right)^2 \right] \int_A |\psi|^2 da$  | resonant cavity p. 67

TE-mode:  $U = \frac{d}{4} \mu \left[ 1 + \frac{\rho\pi}{\delta^2\lambda} \right] \int_A |\psi|^2 da$  | resonant cavity p. 68

The power loss:

$$P_{\text{loss}} = \frac{1}{2\sigma\delta} \left[ \oint_C de \int_0^d dz [\hat{n} \times \vec{H}]_{\text{sides}}^2 + 2 \int_A da [\hat{n} \times \vec{H}]_{\text{end caps}}^2 \right]$$

length of cavity                      end caps

C is circumference

A is cross-section

$\delta$  - skin depth,  $\sigma$ : conductivity

For TH-mode  $\rho \neq 0$

$\hookrightarrow P_{\text{loss}} = \frac{\epsilon}{\sigma\delta\mu} \left[ 1 + \left( \frac{\rho\pi}{\delta^2\lambda} d \right)^2 \right] \left( 1 + \int_{\lambda} \frac{C \cdot d}{4A} \right) \int_A |\psi|^2 da$

dimensionless # of the order of unity

$\hookrightarrow Q = \frac{\mu}{\epsilon c} \frac{d}{\delta} \frac{1}{2 \left( 1 + \int_{\lambda} \frac{C \cdot d}{4A} \right)} = \frac{\mu}{\epsilon c} \cdot \left( \frac{V}{S \cdot \delta} \right) \times (\text{Geometrical factor})$

perm. of metal                      Volume                      surface area

$\hookrightarrow$  Q of cavity is ratio:  $\frac{(\text{Volume occupied by fields})}{(\text{Volume of conductor into which field penetrate})} \times (\text{geometrical factor})$